								Din	nensi	on Ta	ıble								
S x H	12 x 12	12' x 11'	12 x 10	12 x 9	12 x 8	12 x 7	12 x 6	12 x 5	12 x 4	10 x 12	10 x 11	10' x 10'	10' x 9'	10' x 8'	10' x 7'	10 x 6	10 x 5	10' x 4'	S x H
А	37'-0	34'-0	31-0	28'-0	25'-0	22'-0	19'-0	16'-0	13'-0	37'-0	34 -0	31-0	28'-0	25'-0	22'-0	19'-0	16'-0	13'-0	Α
В	12'-4	11'-4	10'-4	9'-4	8'-4	7'-4	6'-4	5'-4	4'-4	12'-4	11'-4	10'-4	9'-4	8'-4	7'-4	6'-4	5'-4	4'-4	В
С	24'-8	22'-8	20'-8	18'-8	16'-8	14'-8	12'-8	10'-8	8'-8	24'-8	22'-8	20'-8	18'-8	16'-8	14'-8	12'-8	10'-8	8'-8	С
C1	25'-6⅓	23'-5%	21-4¾	19'-3%	17'-3	15'-2⅓	13'-1¾	11 0½	8'-11%	25'-6½	23'-5%	21 4 3/4	19'-3%	17'-3	15'-21/4	13'-1⅓	11-0½	8'-11%	C1
C2	25'-31/4	23'-2%	21'-21/8	19-11/4	17'-0¾	14'-11¾	12'-11	10 -10⅓	8'-91/4	25'-31/4	23'-2%	21'-2⅓	19'-11/4	17'-0%	14'-11¾	12'-11	10 -10%	8'-91/4	C2
C3	1%	1½	1%	1%	1%	11/4	11/4	11/4	11/4	1%	1½	1%	1⅓	1%	11/4	11/4	11/4	11/4	C3
DL	10'-3⅓	9'-5⅓	8 71/4	7'-91/4	6 111/4	6 -1 1⁄4	5-31/4	4 -51⁄4	3'-7⅓	10'-3⅓	9'-5⅓	8 71/4	7 91⁄4	6-111/4	6 11/4	5-31/4	4-51/4	3'-7¼	DL
DS	8 111/4	8'-3	7'-61/4	6 91/2	6 0¾	5'-4	4-71/4	3-10%	3'-11/8	8-111/4	8'-3	7-61/4	6'-9½	6 -0¾	5'-4	4-71/4	3 10%	3 -1%	DS
D1	20'-6½	18'-10½	17 - 21/2	15'-6½	13'-10⅓	12'-2½	10'-6%	8'-10%	7'-2%	20'-6½	18'-10½	17'-2½	15'-6½	13-10½	12 - 21/2	10'-6%	8'-10%	7'-2%	D1
D2	7½	6%	6⅓	5%	5	4½	3%	3⅓	2%	7½	6%	61/4	5⅓	5	4½	3%	31⁄4	2%	D2
Е	57'-2%	55'-6⅓	53'-9%	52 -2¾	50'-8	48-111/4	47 -41/2	45 -9⅓	44'-3⅓	51'-2%	49'-6⅓	47'-9%	46 -2¾	44'-8	42 -111/4	41 -4½	39'-9⅓	38'-3⅓	Е
E1	59'-3⅓	57 -5%	55'-81/4	54'-0%	52 -5½	50'-8	49'-0%	47 51/4	45'-9%	53'-0½	51'-3⅓	49'-5%	47 101/4	46 2 1/8	44'-5½	42-10⅓	41 -2¾	39'-71/4	E1
FL	10 -7⅓	9'-91%	8-111/4	8'-11/4	7'-3⅓	6'-5⅓	5-71/4	4'-91/4	3-11½	10 7⅓	9'-9%	8-11⅓	8 -1 ½	7'-3⅓	6'-5⅓	5-71/4	4'-91/4	3-111/4	FL
FS	9-3¾	8'-7	7-101/4	7 -1½	6 4 1/4	5'-8	4-11⅓	4 -2%	3'-51%	9'-3¾	8'-7	7 -10⅓	7 -1½	6 -4 1/4	5'-8	4 111/4	4'-2⅓	3'-5⅓	FS
F1	14 - 31/4	13 -1¾	12 01/4	10-10%	9'-9⅓	8-7½	7'-6	6'-4⅓	5'-2⅓	14-31/4	13 -1¾	12 -0 1/4	10'-10%	9'-9⅓	8 71/2	7'-6	6'-4⅓	5'-2⅓	F1
F2	6-4	5'-10⅓	5'-4⅓	4-10½	4'-4⅓	3'-10⅓	3'-5	2'-111/4	2'-5⅓	6'-4	5'-10⅓	5'-4¾	4-10½	4'-4⅓	3'-10%	3'-5	2'-111/4	2'-5⅓	F2
G	37'-4	37'-2	37'-0	37'-0	37'-0	36'-10	36'-10	36'-10	36'-10	31-4	31'-2	31'-0	31'-0	31'-0	30'-10	30'-10	30'-10	30'-10	G
G1	38'-7¾	38'-5¾	38 - 31/8	38'-3%	38'-3%	38 -1%	38 -1%	38 -1%	38'-1%	32-51/4	32 31⁄4	32 -1⅓	32 -1⅓	32 -1⅓	31-11	31'-11	31'-11	31'-11	G1
G2	39'-10½	39 -8⅓	39 -6%	39'-6¼	39'-6¼	39 -4⅓	39'-4	39 -3%	39-3¾	33'-8	33'-5%	33'-3¾	33-3¾	33-3¾	33 -1%	33'-1½	33 -1%	33 -1⅓	G2
G3	18'-10%	17 -4⅓	15'-10⅓	14 -4⅓	12'-10	11 -3⅓	9'-9¾	8'-3%	6'-9⅓	18 -10%	17 -4⅓	15 -10⅓	14 -4⅓	12'-10	11 -3%	9'-9¾	8'-3%	6'-9%	G3
G4	19'-6⅓	17'-9%	16'-0%	14'-6%	13 -0½	11-3%	9'-9%	8'-3½	6'-9%	19'-6⅓	17'-9%	16'-0%	14'-6%	13'-0½	11 -3%	9'-9%	8'-3½	6'-9⅓	G4
G5	13'-10%	12 -9	11 7¾	10'-6¾	9'-5	8'-3¾	7'-2⅓	6-1	4-11¾	13'-10%	12'-9	11 -7¾	10'-6¾	9'-5	8-3¾	7'-2⅓	6-1	4-11¾	G5
G6	14-111/4	13 -7⅓	12 4⅓	11-3½	10 1 1 1/4	8'-10%	7'-91%	6'-71/8	5'-6⅓	14 111/4	13 -7⅓	12 -4⅓	11 -3⅓	10'-1¾	8'-10%	7'-9⅓	6'-7⅓	5 -6⅓	G6
G7	2%	5¾	81/8	81/8	81/8	10¾	10%	10%	10½	2⅓	5¾	8⅓	81/8	81/8	10¾	10%	10%	10½	G7
G8	3¾	5%	7⅓	7⅓	7½	91/4	91/4	9⅓	9%	3¾	5%	7½	7½	7½	91/4	91⁄4	91⁄4	9⅓	G8
K	38'-0	37-10	37-8	37'-8	37'-8	37-6	37-6	37'-6	37'-6	32'-0	31-10	31-8	31-8	31-8	31-6	31-6	31-6	31-6	K
K1	39'-4⅓	39'-2	39'-0	39'-0	39'-0	38'-9⅓	38'-9%	38'-9%	38'-9%	33'-1½	32'-11½	32′-9¾	32'-9¾	32'-9%	32 -7⅓	32 -7⅓	32'-7%	32 -7%	K1
PL	42'-3%	38'-10%	35'-5½	32 -01/4	28'-7⅓	25'-2	21'-8¾	18 - 3%	14'-10⅓	42'-3%	38'-10%	35'-5½	32'-01/4	28'-71/8	25'-2	21'-8¾	18 - 3⅓	14'-10⅓	PL
PS	37'-0⅓	34'-0	31'-0	28'-0	25'-0	22'-0	19'-0	16'-0	13'-0	37'-0⅓	34'-0	31'-0	28'-0	25'-0	22'-0	19'-0	16'-0	13'-0	PS
RL	44'-1	40'-6⅓	36'-11%	33-41/4	29'-9¾	26 -21⁄2	22 -71/8	19'-0¾	15'-5%	44'-1	40'-6⅓	36'-11⅓	33'-41/4	29'-9¾	26'-2½	22 -71/8	19'-0¾	15'-5%	RL
RS	39'-0⅓	35'-10⅓	32-8⅓	29'-61/4	26'-41/4	23 -2⅓	20'-0¾	16'-10⅓	13-8½	39'-0⅓	35'-10⅓	32'-8⅓	29'-6⅓	26'-41/4	23 -2⅓	20'-0¾	16'-10¾	13-8½	RS
R1	27'-6¾	25'-3⅓	23 -0⅓	20'-8½	18'-5	16'-1⅓	13 - 10 1/8	11 6%	9'-31/4	27'-6¾	25'-3⅓	23′-0⅓	20'-8½	18'-5	16 -1%	13 -10 ⅓	11'-6%	9'-31/4	R1
S1	12'-5%	12 -5⅓	12 -5⅓	12 -5⅓	12 -51/8	12 -5⅓	12'-5⅓	12 -5⅓	12 -5⅓	10'-41/4	10'-41/4	10'-41/4	10'-41/4	10'-41/4	10'-41/4	10'-41/4	10'-4⅓	10'-41/4	S1
Т	1-2	1'-2	1'-2	1'-2	1-2	1'-2	1'-2	1'-2	1'-2	1'-1	1'-1	1'-1	1 - 1	1'-1	1-1	1'-1	1'-1	1'-1	Т
U	1'-0	11	10	10	10	9	9	9	9	1'-0	11	10	10	10	9	9	9	9	U
V	1'-0	11	10	10	10	9	9	9	9	1'-0	11	10	10	10	9	9	9	9	V
V1	1'-0%	11%	10%	10%	10¾	9%	9%	9%	9%	1 -0%	11%	10%	10%	10%	9%	9%	9¾	9%	V1
W	5 -0	4'-9	4'-6	4'-3	4'-0	3'-9	3'-6	3'-6	3 -6	5'-0	4-9	4'-6	4'-3	4'-0	3'-9	3'-6	3'-6	3'-6	W

Notes:

- See Sheet TRFWH G1-21 for General Notes, Specifications, and Design Stresses.
 See Sheet TRFWH 15-1-21 and sheets TRFWH 15-3-21 thru TRFWH 15-6-21 for location of certain dimensions tabulated.

 3. Dimensions are in feet and inches unless otherwise noted.



COUVADOT Highway Division

Standard Design - Triple Reinforced Concrete Box Culverts

Flared Wing Headwalls

February, 2021

Dimension Table 15° Skew

TRFWH 15-2-21

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